which case $0,92 \leqq T_2 \leqq 1$.

When $t \leqq \frac{s}{2}$, then $0,9974 \leqq T_2 \leqq 1$, and (30) can for all practical purposes be reduced to

$$\rho = G\,\frac{V}{I}. \qquad G = \frac{\pi}{\ln 2} \cdot t \cdot C$$

2) Large slice.

The sample is so large that the contour factor C is close to unity. The resistivity may be written:

$$\rho = G\,\frac{V}{I} \qquad G = \frac{\pi}{\ln 2} \cdot t \cdot T_2\left(\frac{t}{s}\right) \cdot C \qquad (31)$$

where:

The thickness factor T_2 is given in section D.2 and the contour factor C is given in sections I.1-4 and K.1 for various configurations.

The condition for C to be close to unity must be decided for each special configuration.

As the factor F(t,c) in formula (29) despicts a second order effect, it will deviate less from unity than C, when C is close to unity.

3) General case.

We must apply the complete expression (29).

$$\rho = G\,\frac{V}{I}, \qquad G = \frac{\pi}{\ln 2} \cdot t \cdot T_2\left(\frac{t}{s}\right) \cdot C \cdot F(t,c)$$

where

the thickness factor T_2 is found in section D.2 and the contour factor C is given in sections I.1-4 and K.1 for various configurations.

F(t,c) is the additional correction factor depending on both thickness and contour. F(t,c) may be smaller and greater than unity, and is generally not known.

When the slice is rectangular, the geometric factor for a bar of rectangular cross section as given in section F.1 may suffice.

When the slice is circular and of thickness $t > s$, the geometric factor can only be estimated by sensible approximations (see sections H.2-4).